



INLAND ENGINEERING & CONSULTING, INC.

Structural & Civil Engineering

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SHT. # 1 OF 8

JOB # 81241

DATE: 2/4/08

STRUCTURAL CALCULATIONS

PREPARED FOR:

SUN TREK

PROJECT:

SOLAR POOL HEATING ATTACHMENT

TRACY, CA. 95376



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DATE _____ SUBJECT _____ SHEET NO. 2
 BY _____ CHKD. _____ JOB NO. 81245

GENERAL INFORMATION:

BUILDING CODE: 2007 CBC

MATERIAL PROPERTIESLUMBER: (STRUC. LUMBER DOUGLAS FIR LARCH)

	GRADE	Fb	Ft	Fv	E	Fc
2x AND 4x JOIST AND BEAM.....	No. 2	875	575	95	1.6×10^6	1300
	No. 1	1000	575	95	1.7×10^6	1300
	SELECT	1450	575	95	1.9×10^6	1300
6x BEAMS & THICKER.....	No. 1	1350	675	85	1.6×10^6	925
6x POSTS.....	No. 1	1350	825	85	1.6×10^6	1000
GLU-LAMINATED BEAMS.....	24-F-V4	2400	1100	165	1.8×10^6	1600
PSL-PARALLAM OR EQ.		2800	1850	285	2.0×10^6	2700

CONC.:	fc	wt.
SLAB ON GRADE.....	2500 psi	150pcf
FOOTING.....	2500 psi	150pcf

MASONRY:

CONC. BLOCK.....1500 psi

REINF. STEEL: # 4 BAR AND SMALLER GR. 40.
 # 5 BAR AND LARGER GR. 60.

STRUC STEEL:

STRUC. PLATES.....Fy = 36 ksi
 PIPE COLS.....Fy = 35 ksi
 STL. TUBES.....Fy = 46 ksi

DATE _____ SUBJECT _____
 BY _____ CHKD. _____

SHEET NO. 3
 JOB NO. 81245

SCOPE OF WORK

SUNTREK'S SOLAR SYSTEM ATTACHMENT ON ROOF

WEIGHT OF SYSTEM : 1.5 PSF FULL

MAX. COLLECTOR SPAN = 70 FT.

DESIGN LOADS:

WIND = 85 MPH EXP. C

ASSUMED HT. OF ROOF 20'

$C_e = .90$

$K_{zt} = 1.0$

$K_d = .185$

$I = 1.0$

$$q_h = .00256 K_z K_{zt} K_d v^2 I$$

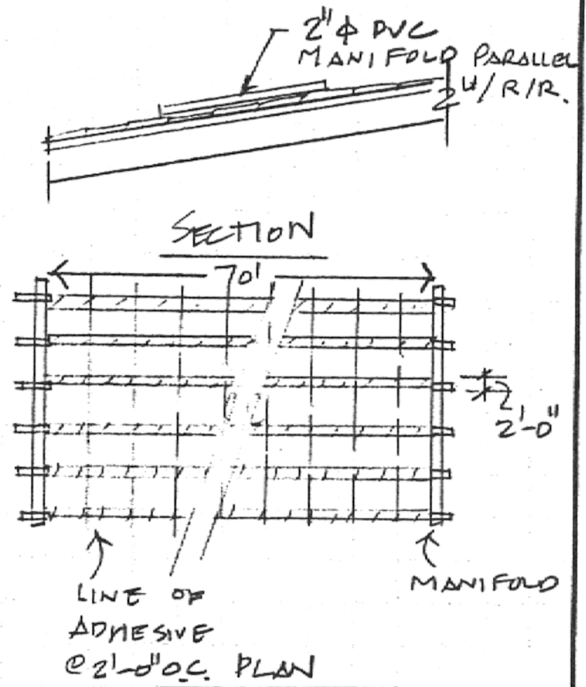
$$= .00256 (.9)(1.0)(.185)(85^2) I$$

$$= 14.15 \text{ PSF}$$

NEGL. EXTERNAL PRESSURE COEFF. FOR $(G_{CP}) = -0.9$

$$P_w = q_h [G_{CP} - G_{pi}]$$

$$P_w = 14.15 [-0.9 - .18] = 15.3 \text{ PSF}$$



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SEIS. LOAD:

$$F_p = \frac{.4 a_p S_{ds} W_p}{(R_p / F_p)} \left(1 + 2 \frac{z}{h} \right) \begin{cases} < F_p = 1.6 S_{ds} F_{pw} \\ > .3 S_{ds} F_{pw} \end{cases}$$

$a_p = 2.5, R_p = 3.0, F_p = 1.0, S_{ds} = \frac{2}{3} S_{MS}, S_{MS} = F_a S_s$ } ZUP. CODE
 $F_a = 1.163, Z = h = 20', S_s = .842$ } 95209

$S_{MS} = (1.0)(.842) = .842$
 $S_{ds} = \frac{2}{3} (.842) = .561$ } SITE CLASS 'D'

$$F_p = \frac{(.4)(2.5)(.561) W_p}{(3. / 1.)} \left(1 + 2 \frac{20}{20} \right) = .561 W$$

$F_{p \text{ MAX.}} = 1.6 (.561) (F_p) W_p = .897 W_p$
 $F_{p \text{ MIN.}} = .3 (.561) (F_p) W_p = .168 W_p$ } OK

NOTES

* COLLECTORS ARE 2'-0" WIDE

* COLLECTORS ARE ATTACHED TO ROOF @ 2'-0" O.C.

T.A. OF COLLECTOR = 2' x 2' = 4.0 SF.

WT. = 4.0 (1.5 PSF) = 6.0 LB. / FT.

WIND LOAD: $F_w = 15.3 \text{ PSF} (6) = 91.8 \text{ LBS. / FT.}$

SEIS. LOAD: $F_s = .561 (6) = 3.37 \text{ LBS. / FT.}$

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BY _____ CHKD. _____ JOB NO. 81245

CHK. ADHESIVE STRENGTH (SUNTREK SEALANT)

BASED ON TEST RESULTS PROVIDED BELOW

AVERAGE TENSILE STRENGTH IS GIVEN AS 8.04 #/IN

 $FL = 24'' (8.04) = 193^{\#} > 91.8^{\#} \quad FS = 2.1 \quad OK$

The following table is a summary of the data collected during our testing:

Substrates (Adherents)	Average Peel Strength (Pounds Per Linear Inch)
Suntrek Rubber Tubing / Ceramic Tile	12.156
Suntrek Rubber Tubing / Composition Roofing	10.996
Suntrek Rubber Tubing / Wood (maple)	8.045

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DATE _____ SUBJECT _____ SHEET NO. 6
 BY _____ CHKD. _____ JOB NO. 21245

CHK. CONNECTION OF 2" φ MANIFOLD :

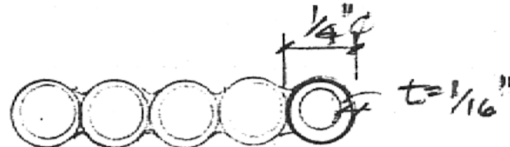
2" φ PVC MANIFOLD ATTACHED EVERY 28" O.C. TO EXIST'G. ROOF TILES FOR TILE ROOFS.

2" φ PVC MANIFOLD ATTACHED EVERY 28" O.C. TO EXIST'G. ROOF RAFTERS FOR SHAKE OR SHINGLE ROOFS.

EA. 2" φ PVC WRAPPED W/ SOLAR PANEL TUBING CONSISTS OF 1/4" φ PLASTIC TUBING (TOTAL OF 5 - 1/4" φ TUBING)



ALLOW. TENSILE STRENGTH = 1479 PSI FOR 1 - 1/4" φ TUBING



$$A = \pi D^2/4 = \pi (.25^2 - .25^2) = .036 \text{ in}^2 \quad \Sigma A = 5 (.036) = .184 \text{ in}^2$$

$$T_{\text{allow}} = 1479 \text{ PSI} (.184) = 272 \text{ PSI} > 91.8 \text{ PSI} \text{ OK}$$

PHYSICALS OF SUNTREK SOLAR TUBE

SAMPLE	SLAB-DUMBBELL	TUBE
DURO, A	80	80
TENSILE STRENGTH, psi	1728	1479
ELONGATION, %	247	224
MOD@25%, psi	355	281
MOD@50%, psi	370	473
MOD@75%, psi	807	686
MOD@100%, psi	1001	899
MOD@200%, psi	1582	1448

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DATE _____ SUBJECT _____ SHEET NO. 7
 BY _____ CHKD. _____ JOB NO. 81245

2" ϕ PVC PIPE SCH. 40 FILLED W/ WATER.
 PIPE #₁ WATER #₁
 $\Sigma W.T. = (3.653 + 1.453) \frac{28''}{12} = 12.8''$ $\frac{28''}{12} = 2.33$ FT.

$F_s = .561(12) = 6.73$ #

$F_w = (2.33)(2) 15.3 = 71.3$ # ← controls

1/4" ϕ LAG SC INTO WOOD RAFTERS MIN. 2" EMB.

$T_{ALL} = 225 \frac{\#}{IN} (2'') = 450$ # > 71.3 # OK

USE 1/4" ϕ WOOD-SC. 2" MIN. EMB. INTO ROOF RAFTERS

CONN. TO ROOF TILES (CONC. TILES)

W/ 1/4" ϕ LAG-SC W/ SET EPOXY TO CONC. TILES



$T_{ALL} = 90$ # > 71.3 # OK

USE 1/4" ϕ LAGS W/ SHIELD EPOXY INTO CONC. TILE

COVER HOLES TO PREVENT LEAKAGE

